

# INSTALLATION • OPERATION • MAINTENANCE I N S T R U C T I O N S

## TYPE HZM DISTANCE RELAY

(WITH OFF-SET TRANSFORMERS—60° TO 90°)

**CAUTION** Before putting protective relays into service, remove all blocking inserted for the purpose of securing the parts during shipment. Make sure that all moving parts operate freely. Inspect the contacts to see that they are clean and close properly, and operate the relay to check the settings and electrical connections.

### APPLICATION

The type HZM relay is a three-unit high-speed relay of the modified zoned distance type operating instantaneously or with a time delay depending upon the location of the fault. The relay is used for phase fault protection on transmission systems and is designed to be used independently or in the high speed carrier relaying system.

The type HZM relay measures the impedance of the line to which it is connected by measuring the ratio of the current and voltage supplied to it. The impedance characteristics may be adjusted and modified so that tripping at the faulted line angle is favored. Thus tripping can be prevented on synchronizing surges of such magnitude that the system will recover, even though the apparent impedance during such surges is considerably below that of the fault impedance. In the same manner tripping under heavy load conditions may be prevented, especially on the longer transmission lines, when the load impedance and the fault impedance are of the same magnitude. The type HZM relay accomplishes this by combining a distance response characteristic with a directional discrimination which can be regulated and adjusted both in magnitude and angle. The directional discrimination is adjusted to produce a high sensitivity at the fault impedance phase angle, but a minimum sensitivity at the load impedance phase angle and at the synchronizing surge impedance phase angles from which system can recover. Therefore this relay with its adjustable

characteristics can be set to fit the particular conditions of the line to be protected.

### CONSTRUCTION

The type HZM relay contains three impedance units, three offset transformers with angular displacement resistors, a synchronous timer, a directional unit, four auxiliary contact switches and three operation indicators.

### IMPEDANCE UNIT

Construction details of these three units are identical and are shown in Fig. 1. A balanced beam is restrained from operating by two voltage coils on the back end, and is pulled downward on the front contact end by a current coil. The fluxes of these two potential coils are shifted out of phase so that practically a constant balance can be obtained regardless of the phase angle between the current and voltage fluxes. A tap screw on the front of the unit permits changing the number of turns on the current coil for coarse adjustments and a core screw on the bottom of the unit changes the current coil electromagnet air gap for the fine adjustment. These two adjustments provide stepless impedance circle radius settings over the one ohm to ten ohms impedance range.

The moving contact is a thin-walled silver shell practically filled with tungsten powder. When this contact strikes the rigid stationary contact, the movement of the tungsten powder creates sufficient friction to absorb practically all of the energy of impact and thus the tendency of the contact to bounce is reduced to a minimum. The moving contact is loosely mounted on the unit beam and held in place by a leaf spring. The construction is such that the beam continues to move slightly after the contacts close deflecting the spring which provides the required contact follow. This spring

**SUPERSEDES I.L. 41-471.1A**

\*Denotes change from superseded issue.

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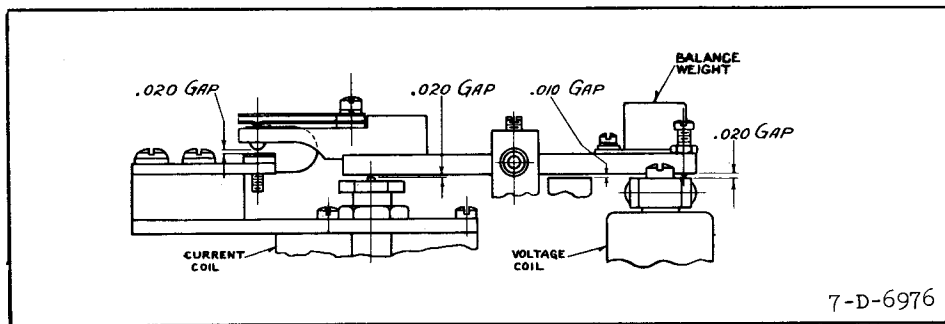


Fig. 1 Sectional View of the Impedance Units.

should have zero tension on the contact when the beam is in the reset position. Current is conducted into the moving contact by means of a flexible metal ribbon.

A thin-walled cylinder filled with tungsten powder is mounted near the rear end of the beam. This acts as a counterweight and tends to damp out vibrations in the beam in the manner described above for the unit contacts.

#### SYNCHRONOUS TIMER

The timer is a small synchronous motor which operates from the current circuit thru a saturating transformer, and drives a moving contact arm thru a gear train. The contact on the moving arm is a cylindrical silver sleeve, loosely fitted on the moving arm. In making contact, this sleeve rolls across two vertically projecting stationary butt contacts to bridge the gap between them. Two sets of stationary contacts are mounted in Micarta insulating blocks which are adjustable around a semi-circular calibrated guide. The maximum time settings are 3.0 seconds for the 60 cycle timer and 3.6 seconds for the 50 cycle timer.

The synchronous motor has a floating rotor which is in mesh with the gear train only when energized. The rotor falls out instantly when the motor is deenergized, allowing a spring to reset the moving arm.

The time delay on the synchronous timer for the second and third impedance units is adjustable from 0 to 180 cycles (50 or 60 cycle basis). T-3 must be set beyond T-2 by a minimum of 25 cycles.

#### DIRECTIONAL UNIT

The directional unit is made up of five basic parts: the die-cast aluminum frame, the

electromagnet, the molded cover assembly, the moving element assembly, and the bridge and upper bearing pin assembly. The lower bearing pin and the magnetic core with its adjustment lever are mounted on the frame. The electromagnet has two series-connected voltage coils mounted diametrically opposite one another, two series-connected current coils mounted diametrically opposite one another and two magnetic plugs accessible through the cover. The moving element consists of a spring and contact arm assembly and a double aluminum loop mounted on a shaft which has end jewels for the top and bottom bearings. This shaft rides between the bottom steel bearing pin mounted in the frame and a similar pin in the bridge that mounts on the two longer studs of the electromagnet. The stops for the moving element are mounted on the cover and are easily accessible for the adjustment of the contact travel. The spring adjuster seats on the molded cover and is attached to the contact through a spiral spring. The moving contact is made of two thin-walled silver shells practically filled with tungsten powder and mounted back to back on a thin leaf spring. The stationary silver contacts are mounted on the molded cover. The electrical connection is made from the stationary contact to the moving contact, through the spiral spring and spring adjuster to the spring adjuster clamp. The magnetic design of the unit is such that the maximum torque occurs when the current leads the voltage 35 to 40 degrees. This is the condition at which the voltage and current fluxes are  $90^\circ$  apart. The flux in each pole face is lagged on the outside edges by copper loops. This produces a torque that counterbalances the centering torque, caused by the small power factor angle of the moving element. The magnetic bias of the unit is controlled by a small lever arm extending to the front on

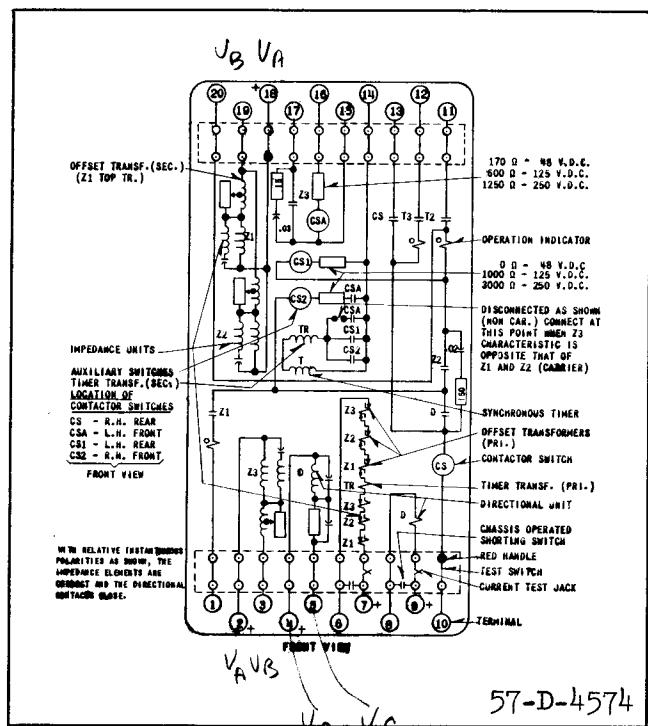


Fig. 2 Internal Schematic of the Type HZM Relay in the Type FT42 Case.

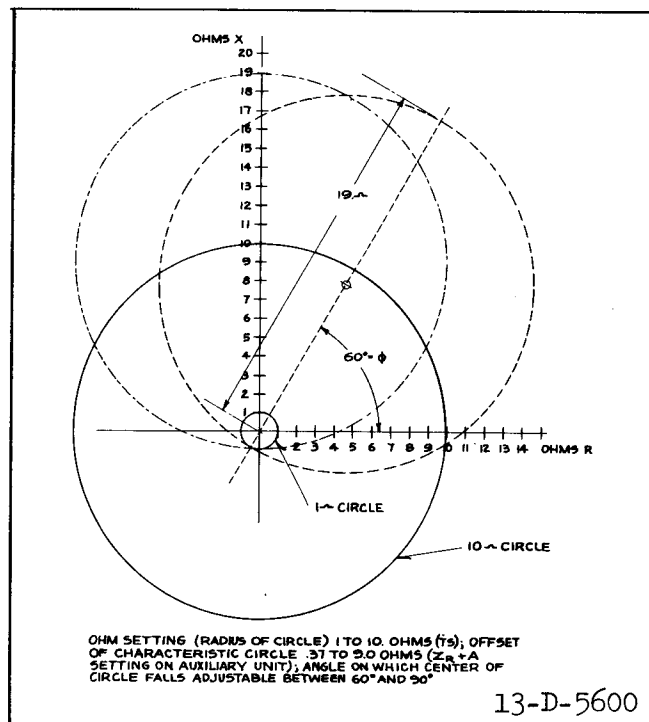


Fig. 3 Operating Characteristics and Ranges of the Type HZM Relay.

the bottom of the unit and two magnetic plugs accessible through the cover. These plugs afford control of the sensitivity at the higher currents.

**AUXILIARY CONTACTOR SWITCHES**

These are small solenoid-type d-c switches. A cylindrical plunger with a silver disc mounted on its lower end moves in the core of the solenoid. As the plunger travels upwards the disc bridges three silver stationary contacts.

**OPERATION INDICATOR**

The operation indicator is a small solenoid coil connected in the trip circuit. When the coil is energized, a spring-restrained armature releases the white target which falls by gravity to indicate completion of the trip circuit. The indicator can be reset from outside of the case.

**OFFSET TRANSFORMERS**

There are three offset transformers with their associated resistors mounted on the back of the sub-base and connected so as to modify the characteristics of the three impedance units. The top transformer is associated with

the first zone, the middle transformer with the second zone, and the bottom with the third zone.

The offset transformer makes it possible to displace the impedance circle characteristic of the impedance unit as plotted on "R" and "X" coordinates, from a circle with the center at the origin to a circle with the center displaced from the origin.

**OPERATION**

The type HZM distance relay is designed to provide a modified operating characteristic that gives improved protection to long transmission lines. One relay is used for each phase.

The impedance relay measures the impedance of the line to which it is connected by measuring the ratio of the current and voltage supplied to it. The relay is connected to receive a current and voltage proportional to those existing on the high-tension line. With a fault in zone 1, Fig. 4, a given amount of current, I, will flow from the relay location to the fault. With zero voltage existing at the fault, phase-to-neutral voltage at the relay location must be equal to the drop in the

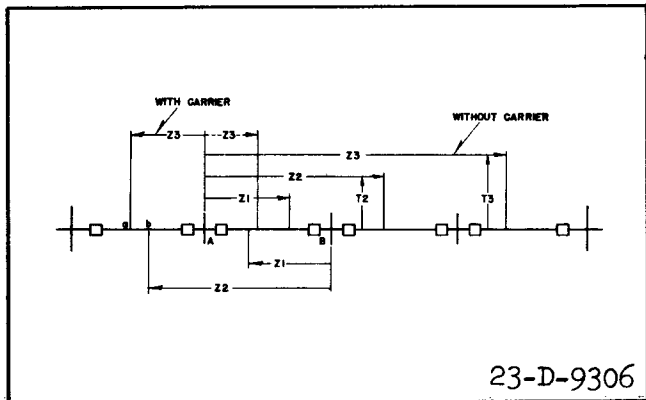


Fig. 4 Typical Settings of the Type HZM Relay in Terms of Line Length.

line due to the current,  $I$ , or equal to  $IZ$  where  $Z$  is the impedance to neutral of the line from the relay location to the point of fault in primary ohms. When considering a three-phase fault, the line voltage would equal  $\sqrt{3} IZ$ , the delta current would equal  $\sqrt{3} I$  and the ratio would be  $\frac{\sqrt{3} IZ}{\sqrt{3} I} = Z$ . When con-

sidering a two-phase fault with zero voltage existing at the fault, the delta voltage of the faulted phases at the relay location equals the voltage drop of the loop or  $I \times 2Z$ , the delta current of the faulted phases equals  $2I$ , and the ratio would be  $\frac{2IZ}{2I} = Z$ . Thus, for

phase faults, the ratio of delta voltage to delta current is used to indicate the location of the fault. This ratio is constant for any value of current as the delta voltage is proportional to the current times the line impedance. By using the turns ratio of the potential transformers and current transformers this  $Z$  can be converted from primary ohms to secondary ohms.

$$Z \text{ secondary} = Z \text{ primary} \frac{R_c}{R_v}$$

Since the relay uses delta voltage and delta current, the  $Z$  relay would equal  $Z$  secondary. Therefore, if the first impedance unit of the type HZM relay with no off-set is adjusted by the core screw and taps on the current coil for a value of current such that the pull of the current coil is just equal to the potential restraint for a fault at the end of zone 1

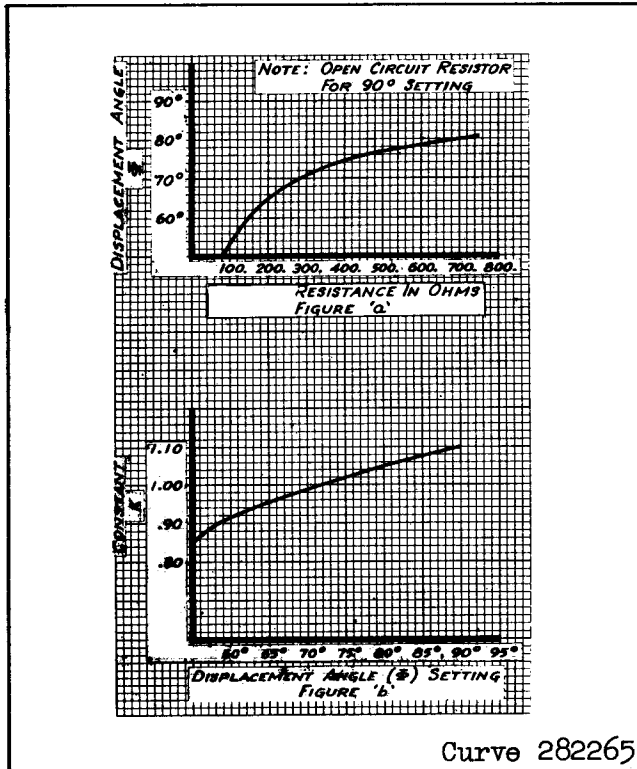


Fig. 5 Adjustment Curve for the Angular Displacement of the Operating Circle Center.

(see Fig. 4), the beam will be balanced for a fault at that point for any value of current. Now, if the fault occurs to the right of this balance point, the beam will not trip as the voltage pull is the greater due to a larger amount of impedance and correspondingly larger potential restraint than the beam is balanced for. The second impedance unit is adjusted to balance for a fault at the end of zone 2; and, therefore operates for faults anywhere up to this point. Likewise, the third impedance unit is adjusted to balance for a fault at the end of zone 3 and operates for faults in all three zones.

The type HZM relay is a modified impedance relay that is identical to the conventional balanced beam impedance relay except that the restraint is produced by the potential and the current instead of by potential alone. The mixing of the current and the potential energy to produce restraint torque is done in the off-set transformer and the resultant energy fed into potential coils of the beam impedance unit. This additional energy will shift the center of the impedance circle away from the

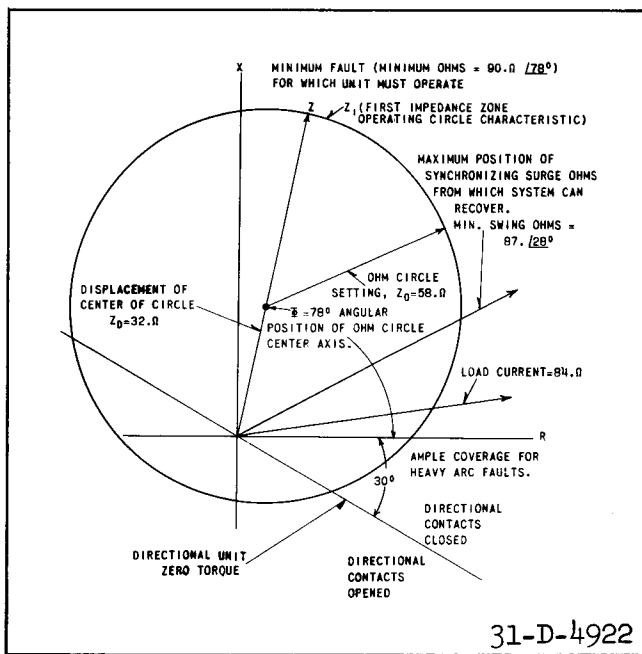


Fig. 6 Transmission Line and Relay Characteristics Plotted on R and X Coordinates in Primary Ohms.

origin of the R-X diagram as shown in Fig. 6. This allows longer settings for the relay without including the swing vector or load impedance vector.

A single-phase directional unit is used in conjunction with the impedance units. The operating range is shown in Fig. 6. For distance relaying, its contacts are so arranged that the portion of impedance circle below the zero torque line is cut off. The directional unit in conjunction with its potential circuit is designed so that the maximum torque occurs when the current leads voltage by approximately 30 degrees. The 90-degree connection is used; hence the voltage circuit receives delta voltage and the current circuit receives the star current that leads this voltage by 90 degrees at 100% power factor. The directional unit closes its contacts when current flows into the line section which is to be protected.

For normal three-zone distance relaying, the trip circuits consist of the following contacts:

- First Zone - directional and first impedance unit contacts;
- Second Zone - directional, second impedance, and first set of timer contacts;

Third Zone - second set of timer contacts. The timer however, will not operate without the directional contacts being closed.

The coil of contactor switch CS is in series with all of the tripping circuits and with the trip coil of the breaker. If the type HZM relays are used without carrier, the contactor switch contacts seal around the relay contacts when the trip circuit coil is energized thereby relieving them of the duty of carrying the tripping current (Fig. 7). These contacts remain closed until the trip circuit is opened by the auxiliary switch on the breaker. The contact operation of this relay with carrier is explained in I. L. 41-904.

### CHARACTERISTICS

The modified characteristic is shown in Fig. 3. A pure impedance unit characteristic plotted on the "R" and "X" coordinates is a circle with the center at the origin. The type HZM relay is so designed that it is possible to displace the center of any impedance circle from the origin and adjust the angle of displacement from 60° to approximately 90°.

There are three variables that can be controlled to fit the transmission line protection requirements making the modified impedance relay very flexible in its applications.

1. The radius of the impedance circle on the "R" and "X" coordinates is entirely determined by the tap (T) and core screw (S) settings of the impedance element.
2. The magnitude of displacement of the center of the impedance circle from the origin is determined by the offset transformer primary tap. ( $Z_R + A$ ).
3. The angle of displacement of the impedance circle can be varied from 60° to 90° current lag by the phase angle adjustment ( $\theta$ ).

The type HZM relay is available in one impedance range 1.0 to 10.0 ohms impedance circle radius (TS) with .37 to 9.0 ohms impedance circle center displacement ( $Z_R + A$ ) over a phase angle from 60° to 90° current lag ( $\theta$ ). All three impedance units are identical and hence have the same range of adjustment. The

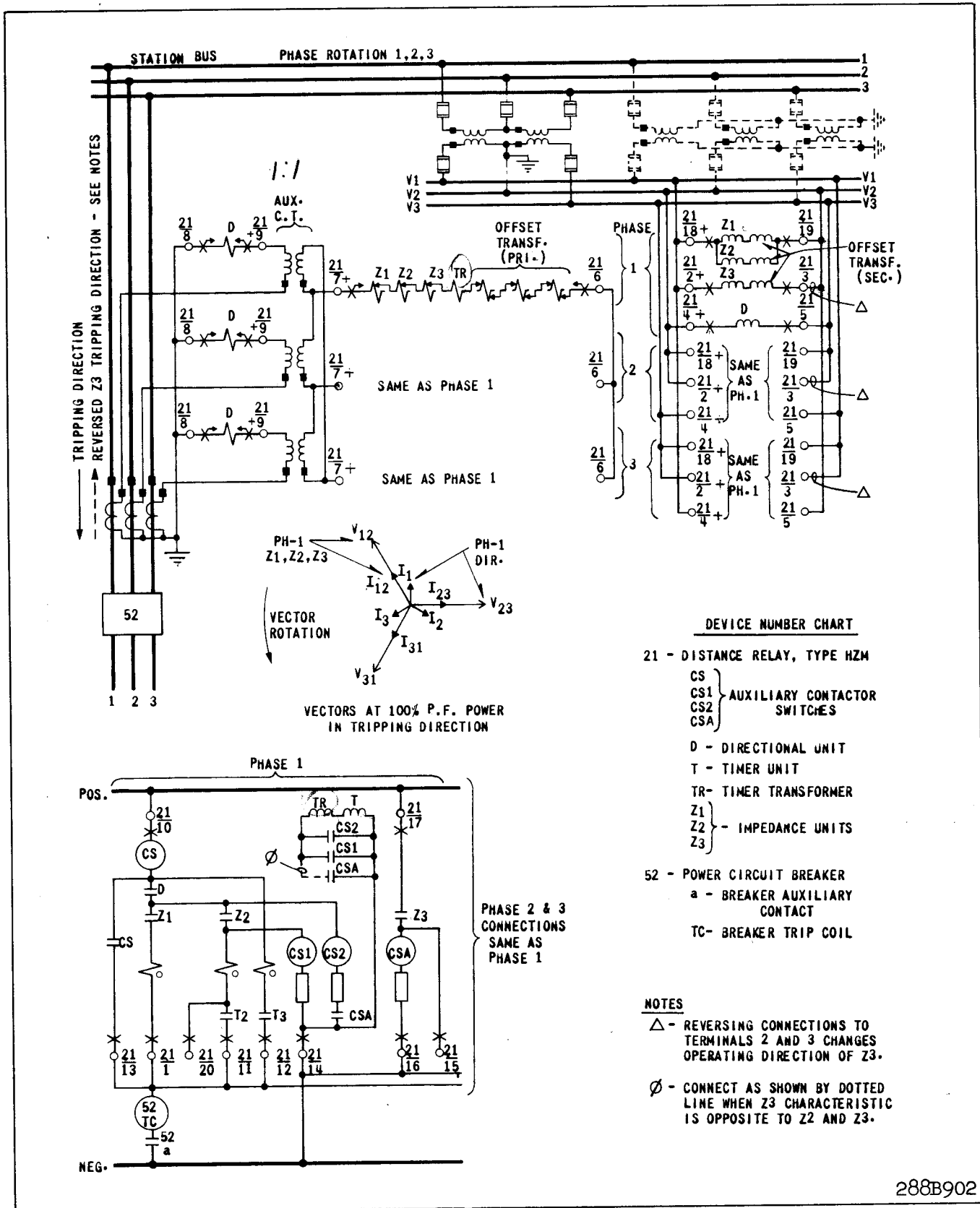


Fig. 7 External Schematic of the Type HZM Relay for Phase Protection of a Three Phase Transmission Line.

tap and scale marking on the relay units are as follows:

(All impedances are in terms in secondary for relay ohms).

Impedance Units (1.0 to 10.0 Ohms)  
Radius of Impedance Circle

TAPS (T)

6.2	9.4	13.5	20.8	29.8	45.
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Core Screw Markings (S)

1.4	1.6	1.8	2.0	2.2
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OFFSET TRANSFORMER

Displacement of impedance circle.

Coarse Ohm Taps ( $Z_R$ )

0.0	1.9	3.7	5.6	7.5
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Fine Ohm Taps (A)

0.0	.37	.75	1.1	1.5
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Phase Angle Displacement ( $\emptyset$ )

60° to 90° Current Lag.

The Phase Angle of Displacement is normally set at 75° unless otherwise specified.

The time delay on the synchronous timer for the second and third impedance units is adjustable in calibrated steps of 20 cycles from 0 to 180 cycles.

Both 50 cycle and 60 cycle relays are available. The relays are not interchangeable as different coils and timers are used.

MINIMUM VOLTAGE REQUIREMENT

The minimum length of line to which the type HZM relay can be applied must be long enough to produce at least  $10 + \frac{100(Z_R + A)}{TS}$  volts on the relay when a fault occurs at the balance point. If the voltage becomes much less than this value, the forces become too small to

assure fast and positive action.

**SETTINGS**

The type HZM relay requires a setting for each of the three impedance units and the synchronous timer for Second and Third Zone time.

Z = line-to-neutral ohmic impedance of the protected line from the relay to the desired balance point in terms of primary ohms.

For the First Unit - 70 to 80% of the protected section.

For the Second Unit - Approx. 50% into the adjacent section.

For the Third Unit - Approx. 25% into the third line section (without carrier).

When carrier is used, see the following section entitled "HZM Carrier Setting of Z3".

When the balance impedance has been determined, the phase angle and magnitude of the minimum load ohms and the phase angle and magnitude of the minimum synchronizing surge ohms from which the system can recover should be determined or estimated to complete the analysis.

It will expedite the application by plotting the transmission line characteristics on "R" and "X" coordinates. An operating circle should then be drawn of a diameter and location to fulfill the following conditions:

1. The circle must pass through the point of the vector Z and must completely enclose the vector Z. (See Fig. 6.)
2. The circle must not enclose the point of the vector of minimum load ohms or of minimum synchronizing surge ohms from which the system can recover.
3. The angular displacement of the center of the circle must be within 60° to 90° current lagging phase angle. This angle is set at 75° and generally it is not necessary to adjust to other angles.

The radius of the circle in ohms should be measured and the impedance unit set in accord-

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ance using the formula:

$$TS = \frac{10Z_o R_c}{R_v}$$

where

T = The impedance unit current tap value.

S = The impedance unit current core screw value. The values appear as a series of dots on the drum of the lower core screw adjusting knob.

$Z_o$  = Radius of circle, as determined in the preceding paragraphs, in ohms primary.

$R_c$  = The current transformer ratio.

$R_v$  = The potential transformer ratio.

The tap, T, is obtained by dividing the TS product by S to give an available tap number. When changing taps with the relay energized, the extra tap screw should be screwed in the desired tap before removing the existing tap screw to prevent open circuiting the current transformers.

The numbers on the core screw appear in ascending order as the core screw is screwed into the core. In some cases, a question of doubt may arise whether the scale setting is correct, or is out by one full turn of the core screw. In such a case, the point may be verified by turning the core screw all the way in. Then back out the core screw until the highest scale marking just comes under the end of the pointer. This will occur in approximately one turn. Then turn to correct setting. Sufficiently accurate setting can be made by interpolating between the marked points when necessary.

From the operating circle, previously constructed, measure the displacement of the center of the circle from the intersection of the "R" and "X" axis in magnitude and angle.

The offset transformer should be set in accordance with the formula:

$$Z_R + A = \frac{Z_D R_c}{R_v K}$$

where

$Z_R + A$  = Offset transformer tap values.

$Z_D$  = Displacement of the center of the operating circle in ohms primary.

K = Constant determined from curve Fig. 5b.

$R_c$  = The current transformer ratio.

$R_v$  = The potential transformer ratio.

$\emptyset$  = Angular displacement.

Normally the  $Z_D$  setting is from 0 to 75% of the  $Z_o$  setting. The angular displacement ( $\emptyset$ ) may be varied by adjusting the resistor above the offset transformer in accordance with the curve of Fig. 5a for a fault at the desired balance point.

- \* As an example of the formula setting, set the first impedance unit to protect a 78° - 110 KV line, 143 miles long. The line-to-neutral impedance is .79 ohm per mile. The current transformer ratio 600/5, and the potential transformer ratio is 1000/1. The first unit is to protect 80% of the line section or for a balance point  $.80 \times 143 \times .79 = 90$  ohms. The phase angle and the magnitude of the minimum synchronizing surge ohms from which the system can recover should be determined.

Plot the transmission line characteristics on "R" and "X" coordinates as shown in Fig. 6. An operating circle should then be drawn of a diameter and location to fulfill the conditions previously stated.

The radius of the circle in ohms should be measured and the impedance unit set in accordance using the formula:

$$TS = \frac{10Z_o R_c}{R_v}$$

$$TS = \frac{10 \times 58.0 \times 600/5}{1000/1} = 69.6$$

T will be set on 45 (Relay Tap Setting)

S will be set on 1.55 (Relay Core Setting)

The displacement angle used in drawing the operating circle should be set on the relay by adjusting the resistor mounted above its offset transformer in accordance with the curve of Fig. 5a. In Fig. 6 the angle used was 78 degrees; therefore, the resistor should be



adjusted to 600 ohms.

The distance expressed in ohms impedance between the center of the modified impedance circle and the intersection of the "R" and "X" axis should be measured from Fig. 6, and the offset transformer set using the following formula:

$$Z_R + A = \frac{Z_D R_C}{R_V K}$$

$$Z_R + A = \frac{32 \times 600/5}{1000/1 \times 1.04} = 3.69 \text{ ohms}$$

$Z_R$  should be set on 3.7 ohms.

A should be set on 0 ohm.

The setting for the second and third impedance unit is obtained in the same manner as the preceding example for the first impedance unit.

The time delay on the synchronous timer is set to coordinate with the relays which are backed up by the second and third impedance unit. The setting is made by moving the complete contact assembly to the desired position as indicated by the scale.

On lines where taps or parallel feeders supply fault power to the adjacent sections, the apparent impedance to the relay backing up the adjacent section is greater than the actual impedance. The reason for this is that the relay does not receive the additional fault current supplied by the other feeders, but at the same time, this current does increase the voltage drop from the fault to the relay. This increases the apparent impedance to the adjacent section by the ratio of the total current to the relay current. The effect on the relay impedance units is to back up the balance point of the second and third impedance units. In order to extend the range of back-up protection under these conditions, the second unit can be set for a balance point farther than the 150% normally recommended, provided it is made to time select with the adjacent section relay second unit. Similarly, the third unit can be set farther than normal if it is made to select with the second and third units of the adjacent relay which it overlaps.

\* The formula settings are sufficiently accurate for most installations. Where it is desired to set the balance point more accurately the tap and scale values may be checked by applying to the relay the voltage, current, and phase angle conditions which will be impressed on it for a fault at the desired balance point. A slight change in the scale value from that calculated may be required so that the relay will just trip for the simulated fault at the balance point.

The particular setting of one unit may have some influence on the adjacent unit. The factory calibration of the core screw is made with taps cascaded as indicated in the section, "Electrical Check Points."

The numbers on the core screw appear in ascending order as the core screw is screwed into the core. In some cases, a question of doubt may arise whether the scale setting is correct, or is out by one full turn of the core screw. In such a case, the point may be verified by turning the core screw all the way in. Then back out the core screw until the highest scale marking just comes under the end of the pointer. This will occur in approximately one turn. To prevent such doubt it is recommended that the core screw setting be made by thus locating the highest scale marking and then continuing to back it off until the desired value appears exactly under the end of the pointer. Sufficiently accurate setting can be made by interpolating between the marked points when necessary.

#### HZM CARRIER SETTING OF Z3

When the type HZM relay is used with carrier, the third zone unit must operate in a reverse direction from Z1 and Z2 whenever the modified distance characteristic is used. This is done to assure proper carrier blocking for external faults in the adjacent line section with a setting of Z3 which will not pick up on load or surge ohms. This may be accomplished by merely reversing the polarity of the Z3 potential circuit.

The method of arriving at the proper setting is shown in Fig. 4 which also shows the normal settings of Z1, Z2, and Z3 when used without carrier. When the HZM relay is used with carrier, the ohmic reach of Z3 at station A in

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the direction away from line AB should be greater than the reach of Z2 (from station B) past the local station bus (at A). Thus any fault in the zone Ab which picks up Z2 at B will also pick up Z3 at station A to block tripping at B. The zone ab is for a safety factor to insure that carrier will always be started at A before carrier tripping can be set up at B. For this service, Z3 should be set to reach out of the line 50% farther than the reach of Z2 (at B) past the station A Bus. In Fig. 4, this means Aa should be 150% of Ab. The reach of Z3 into the line section AB as shown is not critical, but should be at least 20 per cent of the offset ohms.

When the Z3 setting is reversed, the second contact of the CSA must be connected in parallel with the CS1 contact to control the timer. This provides third zone back-up protection for lines away from the line protected by zone one and two. Thus the timer is controlled by Z2 and D or Z3 only.

### INSTALLATION

The relays should be mounted on switchboard panels or their equivalent in a location free from dirt, moisture, excessive vibration, and heat. Mount the relay vertically by means of the four mounting holes on the flange for semi-flush mounting or by means of the rear mounting stud or studs for projection mounting. Either a mounting stud or the mounting screws may be utilized for grounding the relay. The electrical connections may be made directly to the terminals by means of screws for steel panel mounting or to the terminal studs furnished with the relay for thick panel mounting. The terminal studs may be easily removed or inserted by locking two nuts on the stud and then turning the proper nut with a wrench.

For detailed FT case information refer to I.L. 41-076.

### CONNECTIONS

#### IMPEDANCE UNITS

The impedance to the balance point is measured from the point where the potential transformers are connected to the protected line. For protecting transmission lines, the relays

should receive potential from potential transformers connected directly to the line at the point from which the impedance is to be measured.

In some applications, a power transformer bank forms part of the transmission line, and potential transformers are available only on the bus side of the bank. In this case the relays may be set thru the bank to protect the line only if the bank impedance is not too large as compared with the line impedance. If the bank impedance is too large in comparison with the line impedance, the 70 or 80% setting of the first unit may cover only a very small percentage of the transmission line or in some cases not cover any of the line section. For the same reason, the second and third units will offer considerably less back-up protection over the adjacent lines. In order to use the potential transformers on the bus side of the bank under this condition, Type KX compensators are used and the impedance is measured from the line side of the bank to the balance points. The type KX compensators operate from the current transformers and provide voltage compensation equivalent to the drop in the power bank. The setting of the KX compensator is covered by I.L. 41-861.

The above discussion assumes that power is fed thru the bank to faults on the line. Where a power transformer connects to a high-tension transmission line and does not supply power to the line fault, low-tension potential transformers may be used without compensation. Then, the impedance to the balance point is measured from the point where the power bank connects to the protected line.

The conventional star connection of current transformers is not satisfactory where accurate distance relay protection is desired. With this connection the balance points of the impedance units shift about 15% depending upon whether a phase-to-phase, a three-phase, or a double-line-to-ground fault is involved. That is, if the balance point were adjusted at 80% for a three-phase fault, then for a double-line-to-ground fault the shift may be more or less than plus or minus 15% of the 80% setting, depending upon the ratio of the zero sequence impedance to the negative sequence impedance of the system from the source of power to the fault. This error can be entirely eliminated

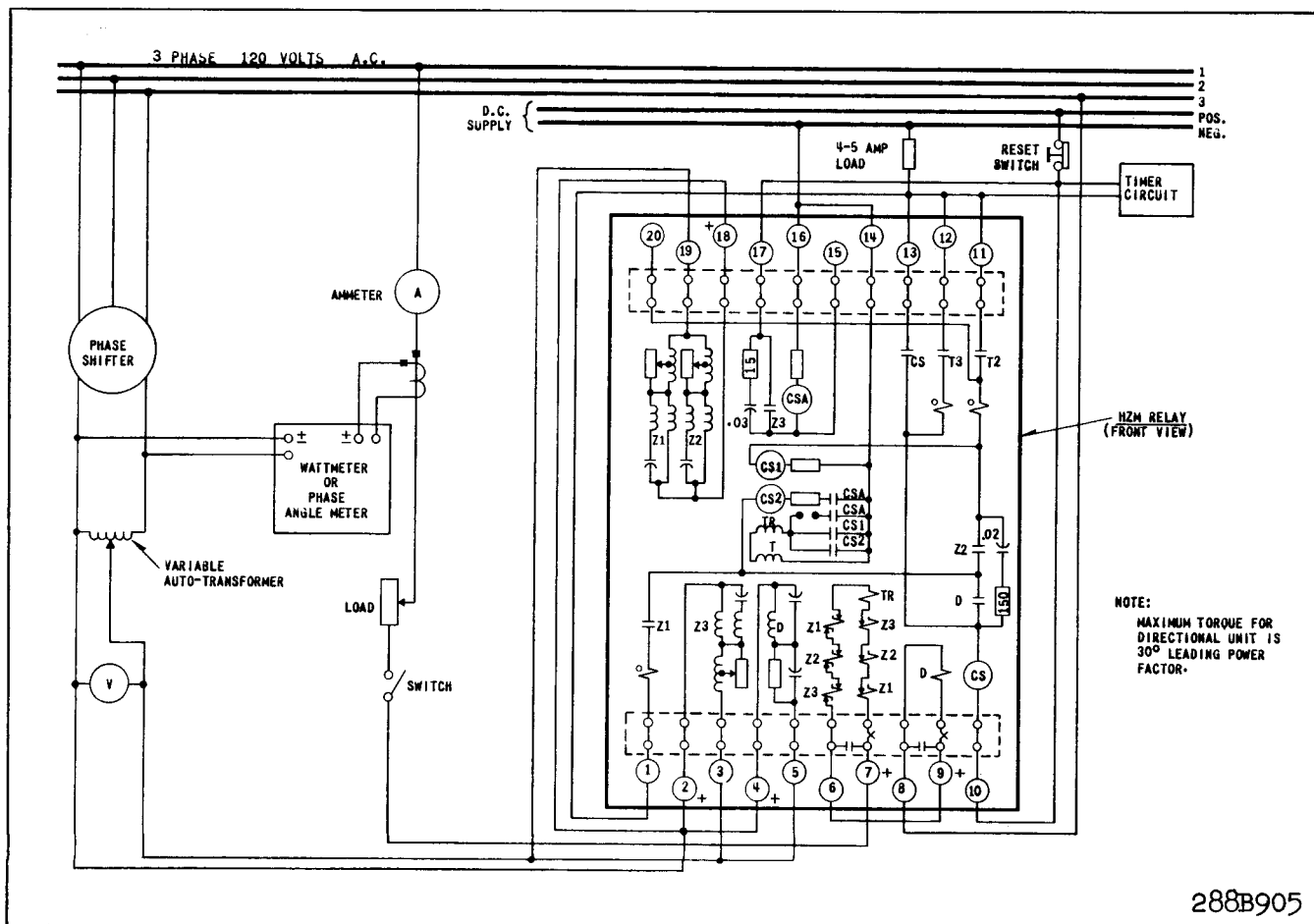


Fig. 8 Diagram of Test Connections for the Type HZM Relay.

by making use of the vector difference between the line current; i.e., delta currents, for actuating the relay.

The most common method is to connect the main current transformer in star and use a set of auxiliary 5/5 ratio transformers to supply delta currents to the impedance units as shown in Fig. 7.

The delta voltages used on the impedance units of the relays should be in phase with the delta currents, at unity power factor.

DIRECTIONAL UNIT

The magnetic design of the unit and potential circuit is such that maximum torque occurs when the current leads the voltage by approximately 30 degrees. Thus, the directional unit coils should be connected to receive current that leads the voltage by 90 degrees when the line power factor is 100 percent. This will result in operation at approximately the maximum torque angle for transmission line faults.

TRIP CIRCUIT

The contactor switch operates on a minimum of 1.0 ampere, but the trip circuit should draw at least 4 or 5 amperes in order to reduce the time of the operation of the switch to a minimum and provide more positive operation. If the type HZM relay is used to trip an auxiliary multi-contact relay, provision should be made for loading down the trip circuit with a resistor in parallel with the operating coils of the auxiliary relay. Also, since the total trip circuit resistance in the relay is approximately 1.0 ohm, care must be taken to see that the breaker trip coil will receive enough current when low voltage control is used.

The main contact on the impedance units and directional unit will safely close 30 amperes at 250 volt d-c., and the switch contacts will safely carry this current long enough to trip a breaker.

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## ELECTRICAL CHECK POINTS

To check the electrical operation of the relay, the following instruction should be followed.

Connect the relay per Fig. 8 and make the following settings. (At regular maintenance periods the settings of each particular relay with the voltage and current expected at the balance point should be used, if available. During factory testing, the settings are cascaded as indicated below.)

IMPEDANCE UNIT			OFFSET TRANSFORMER		
Zone	T	S	Z <sub>R</sub>	A	∅
Z <sub>1</sub>	20.8	1.8	1.9	0.0	75°
Z <sub>2</sub>	29.8	1.8	3.7	0.0	75°
Z <sub>3</sub>	45	1.8	5.6	0.0	75°

**CAUTION:** The relay voltage should be of good wave form. The combination of a phase shifter and autotransformer may give an output voltage of poor wave form if the magnetizing current of the autotransformer is high in proportion to the impedance of the phase shifter used. In case of doubt, check the output voltage wave form with an oscilloscope.

### DIRECTIONAL UNIT

With 120 volts and 5 amperes in phase, the directional element should be closed. The contacts should open when the current leads the voltage by approximately 120 degrees or lags the voltage by approximately 60 degrees.

### IMPEDANCE UNITS

With 60 volts on the relay, increase the current until the contacts just close. This current (which will vary slightly from this value if suddenly applied) should be approximately:

- Z-3 I = 4.4 amps. at 75° lag I (non-carrier)
- Z-3 I = 4.4 amps. at 255° lag I (carrier)
- Z-2 I = 6.6 amps. at 75° lag I
- Z-1 I = 10.5 amps. at 75° lag I

With the D contact closed, the tripping of Z-3 should cause CSA switch to pick up, and CS-1 switch in turn. When Z-2 trips, the CS-2 should pick up. The operation of CS1 or CS2 should start the timer. When Z-1 trips or the timer T-2 or T-3 contacts close, the CS switch

should operate and seal around all the contacts. The CS, CS-1 and CS-2 are not continuously rated; therefore, care should be taken not to overheat these auxiliary switches. The checking of the timer unit will depend on the standard time device used. Generally this check is made independently of the trip circuit to avoid circuitry complications. The timer should operate with 3.5 amperes in the timer transformer and with the contacts of CS-1 (or CS-2) closed or shorted. An auxiliary relay as used in the trip circuit should be used to seal in the timer circuit.

## ADJUSTMENTS AND MAINTENANCE

The proper adjustments to insure correct operation of this relay have been made at the factory and should not be disturbed after receipt by the customer. If the adjustments have been changed or the relay taken apart for repairs, or if it is desired to check the adjustments at regular maintenance periods, the instructions below should be followed.

All contacts should be cleaned periodically. A contact burnisher S#182A836H01 is recommended for this purpose. The use of abrasive material for cleaning contacts is not recommended, because of the danger of embedding small particles in the face of the soft silver and thus impairing the contacts.

### IMPEDANCE UNITS

The voltage circuit on the impedance units is designed to have a comparatively flat phase angle curve. This is accomplished by energizing the two coils with currents that are essentially equal and 90° out of phase. The gaps as shown in Fig. 1 are nominal dimensions which yield equal restraints from the two coils. The actual gaps on any particular relay may vary a few thousandths from these values.

If the voltage circuits have been disassembled, the gaps referred to in Fig. 1 provide a nominal starting point for calibration. This is accomplished as follows:

1. Adjust the stop screw on the rear of the beam to give a clearance of .020 inch between the beam and the voltage iron circuit. With the beam in the reset position, i.e., with the stop screw against the stop, adjust the vertical gap for .010 inch between the adjustable iron and the beam. Also, with the beam in the

same position, adjust the gap between the front end of the beam and the stop in the upper screw to .020 inch.

Further adjustment in the gaps may be necessary to obtain a reasonably flat phase angle curve at 100 volts.

The first and second impedance unit beams should be balanced as follows. Connect the relay with polarities as shown in the test diagram, Fig. 8. Set the offset transformer taps  $Z_R$  and A on zero and  $\emptyset$  on any setting. With any tap and scale setting, check the impedance measured by the relay with 60 volts potential restraint. Apply 10 volts restraint and adjust the balance weights on the beam until the beam just trips with 1/6 of the current required to trip with 60 volts restraint. The current should be suddenly applied.

The third impedance unit beam should be balanced by adjusting the balance weight so that in the de-energized condition, the beam will reset, thus leaving its contact open. Do not introduce excessive resetting torque, but only enough to reset the unit.

The stationary contact should be adjusted for a .020 inch gap when the beam is in the reset position. When the beam is in the operated position, there should be a .015 inch deflection of the moving contact. The spring that carries the moving contact should lie flat on the Micarta arm with no initial tension on the contact. The flexible pigtail should be at least 3/32 inch from the end of the stationary contact.

With the taps set on 45 and 60 volts applied to the potential circuit, remark the core screws (or check the markings) so that the current to trip the beam at  $75^\circ$  lag will satisfy the formula

$$\frac{E}{I} = \frac{TS}{10}$$

The "S" markings should be as shown under characteristics of the relay.

The offset of the impedance circle can be checked by setting  $Z_R + A$  to any value with  $\emptyset = 75^\circ$ , and seeing that the current to trip the beam at  $75^\circ$  lag satisfies the equation

$$\frac{E}{I} = \frac{TS}{10} + (Z_R + A) K$$

### DIRECTIONAL UNIT

The upper bearing screw should be screwed down until there is only three to four thousandths of an inch clearance between it and the shaft, and then securely locked in position with the lock nut. This adjustment can be made best by carefully screwing down the top bearing screw until the double loop fails to turn freely and then backing up 1/8 of a turn. Great care must be taken in making this adjustment to prevent damage to the bearings.

The front contact spring should be positioned in the center of the .020 inch slot of the aluminum guard by means of the small adjusting screw located on the nut plate that holds the spring on the moving element. The travel of the moving contact is limited by the stationary contacts mounted on the molded cover. The contact gap should be adjusted as follows: With the moving contact centered between the studs, close the contact gaps by advancing the two front stationary contacts. Then back off the right-hand stationary contact .035 inch and lock both contacts in place. The complete moving element is limited in travel by two stop screws, located on the molded cover. These should be adjusted so that the moving contact just barely misses the stationary contact stops front and rear respectively when energized in the opening and closing directions with 120 volts and 5.0 amperes at maximum torque. The right-hand stationary contact should just touch the moving contact when energized as above and then should be turned 1/6th of a turn to obtain .005 inch contact follow. Too much follow should be avoided to insure proper coordination. The spring should be adjusted so that the contact closes with approximately 1.0 volt and 5 amperes at maximum torque.

- \* A small lever arm extending to the front on the bottom of the unit and the plugs accessible through the molded cover control the magnetic bias of the electromagnet. The lever should be adjusted so that the unit will operate with 40 amperes and 0.2 volt at the maximum torque angle. Before or after this adjustment, short the voltage coils and check to insure that the contacts do not close on 60 amperes momentarily applied. Raising the right-hand plug under these conditions will produce torque to the right when considering the front moving contact.

## TYPE HZM RELAY

The unit can be adjusted to just remain open under these conditions or adjusted to operate with 75 amperes and 0.2 to 0.4 volt at the maximum torque angle.

### CONTACTOR SWITCH (SEAL-IN SWITCH) CS

Adjust the stationary core of the switch for clearance between the stationary core and the moving core of .025 inch when the switch is picked up. This can be done by disconnecting the switch, turning it up-side-down and screwing up the core screw until the contact just separates. Then back off the core screws approximately one turn and lock in place. This prevents the moving core from striking and sticking to the stationary core because of residual magnetism. Adjust the contact clearance for 3/32 inch by means of the two small nuts on either side of the Micarta disc. The switch should pick up at 1.0 ampere direct current. Test for sticking after passing 30 amperes direct current through the coil.

### CONTACTOR SWITCH CSA

The adjustments are the same as for the seal-in contactor switch "CS" except that the contact clearance should be 1/32 inch. For 125 volt d-c relays, apply 80 volts d-c to Nos. 16 and 17 terminals. Similarly for 250 volt d-c relays, apply 160 volts d-c to Nos. 16 and 17 terminals. See that the switch picks up and closes its contacts positively when the contact of the third impedance unit is made. The switch coil is continuously rated.

### CONTACTOR SWITCHES CS-1 AND CS-2

The adjustments are the same as for the seal-in contactor switch CS except that the contact separation should be 1/32 inch. For 125 volt d-c relays, apply 60 volts dc positive to Nos. 10 and 17 terminals and negative to Nos. 14 and 16 terminals. Similarly for 250 volt d-c relays, use a test voltage of 120 volts d-c. See that switch CS-1 picks up and closes its contact positively when the directional and Z-2 impedance unit contacts are made. See that CS-2 picks up and closes its contacts when the directional unit and Z-3 impedance unit contacts are made. These switch coils are intermittently rated, and therefore care should be exercised so as not to over-

heat the coils.

### OPERATION INDICATOR

Adjust the indicator to operate at 1.0 ampere direct current gradually applied. Test for sticking after passing 30 amperes direct current through the coil.

### SYNCHRONOUS TIMER

When testing the synchronous timer, complete the transformer circuit by a jumper around the contacts on the contactor switch CS-1 or CS-2 rather than operating the switch on d-c. Test the motor with 3.5 amperes through the current circuit of the relay. This is the minimum current at which it will run in synchronism.

### TIMING TESTS

The d-c trip circuit should be loaded with a resistor to draw approximately 5 amperes and an auxiliary relay should be used to operate the timer circuit if time tests are to be taken. There is a slight vibration of the beam and contacts because of the pulsating pull on the current side of the instantaneous unit. This vibration may prevent positive stopping of the timing device unless an auxiliary type MG relay is used. The loading resistor will cause the contactor switch to seal-in and simulates the actual service condition when a circuit breaker is to be tripped. This type of circuit is also necessary when timing T-2 or T-3.

**CAUTION** Make certain that the stops on the rear and front of each beam are absolutely clean otherwise the impedance at which the beam trips may be affected, particularly at low voltages. The stop can be easily cleaned by drawing a piece of clean white paper between the beam and the stop while the beam is firmly pressed down.

### RENEWAL PARTS

Repair work can be done most satisfactorily at the factory. However, interchangeable parts can be furnished to the customers who are equipped for doing repair work. When ordering parts, always give the complete nameplate data.

## ENERGY REQUIREMENTS

Typical burden data of the various circuits are as follows:

Potential Circuits at 120 Volts, 60 Cycles

<u>Circuit</u>	<u>V. A.</u>	<u>P. F. Angle</u>
All Impedance Circuits		
Displacement angle $90^\circ$	7.2	$48^\circ$ lag
Displacement angle $60^\circ$	6.8	$29^\circ$ lag
Directional unit	6.6	$19^\circ$ lead

Potential Circuits at 120 Volts, 50 Cycles

<u>Circuit</u>	<u>V. A.</u>	<u>P. F. Angle</u>
All Impedance Circuits		
Displacement Angle $90^\circ$	6.5	$40^\circ$ lag
Displacement Angle $60^\circ$	6.0	$22^\circ$ lag
Directional Unit	6.4	$9^\circ$ lead

Current Circuits at 60 Cycles+

<u>Circuit</u>	<u>Amps.</u>	<u>V. A.</u>	<u>P. F. Angle</u>
Impedance Circuit			
T = 45, S = 1.8			
$Z_R = 7.5$ A = 0.0	8.66	36.0	$50^\circ$ lag
T = 13.5, S = 1.4			
$Z_R = 0.0$ , A = 1.1	8.66	17.0	$50^\circ$ lag
Directional Unit	5	2.0	$50^\circ$ lag

+The burdens of the current circuits, at 50 cycles, are slightly less than the above values.

**TYPE HZM RELAY**

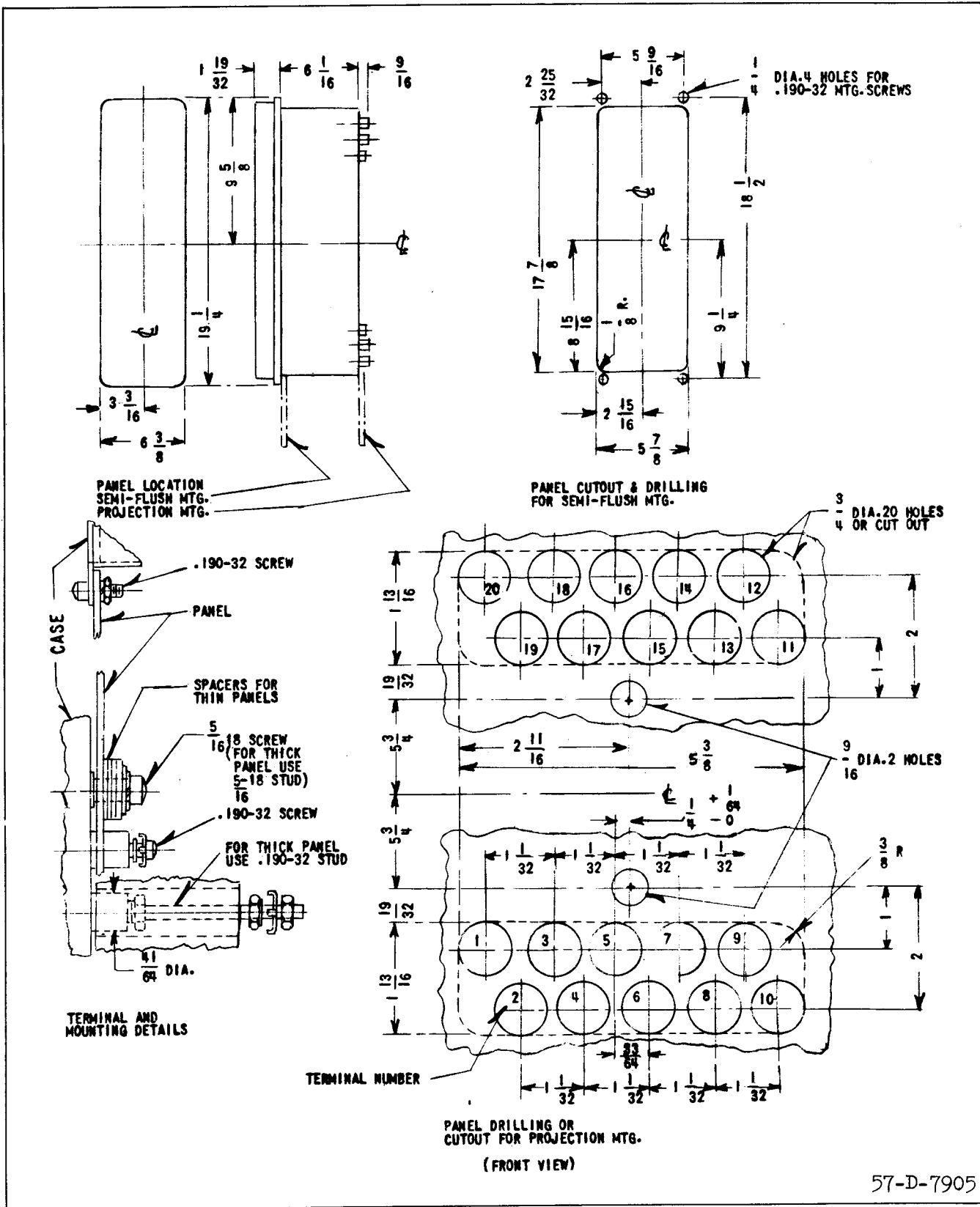


Fig. 9 Outline and Drilling Plan of the Type HZM Relay in the Type FT42 Case.

**WESTINGHOUSE ELECTRIC CORPORATION**  
**RELAY-INSTRUMENT DIVISION**

**NEWARK, N. J.**

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